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Design And Analysis Of Two Wheeler Suspension System By FEA Approach

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Abstract - The Suspension system is the most important part in any vehicle. It handles shock impulse and dissipates kinetic energy. It reduces the amplitude of disturbances and improved ride quality. The spring is compressed quickly when the wheel strikes the bump. The compressed spring rebound to its normal dimension when load is removed. The spring goes down below its normal height when the weight of the vehicle pushes the spring down. This, in turn, causes the spring to rebound again. The spring bouncing process occurs over and over every less each time, until the up-and-down movement finally stops. The vehicle handling becomes very difficult and leads to uncomfortable ride when bouncing is allowed uncontrolled. Hence, the designing of spring in a suspension system is very crucial. The present work is carried out on helical spring where, modelling, analysis and testing of suspension spring is done to replace the existing design of helical spring used in popular two wheeler vehicle. The different designs of springs are modelled by reducing the diameter of the existing spring. The analysis is carried out by considering bike mass, loads, and no of persons seated on bike. The stress and deflections of the helical spring are determined by using finite element analysis approach. The comparative study is carried out between baseline spring and new design of spring by constant material. The results from finite element analysis are compared to the experimental values. A typical two wheeler suspension spring (spring for Hero Splendor 125 cc) is selected for the application. The solid model of spring is developed in CATIA and the analysis part is carried out in ANSYS.

Key Words: Helical Spring, Finite Element Analysis, CATIA, ANSYS

I. INTRODUCTION

The aim of this project is to contribute to the development of an enhanced automotive coil springby evaluating existing manufacturing processes and relating this to fatigue properties and residual stresses in the components. The development of a coil spring that is 15% lighter and which can operate at 20% higher stresses will bring about a major revolution in the manufacturing of automotive suspensions. This could result not only in a lighter vehicle but also a reduction in space required by suspensions, which could open the way for new, less drag resistant front body panels. In vehicle suspension system, helical compression coil spring is one of the primary elastic component.

A spring is an elastic body, whose function is to distort when loaded and to recover its original shape when the load is removed. It is an elastic object used to store mechanical energy. Springs are usually made out of spring steel. Small springs can be wound from pre-hardened stock, while larger ones are made from annealed steel and hardened after fabrication. Some non-ferrous metals are also used including phosphor bronze and titanium for parts requiring corrosion resistance and beryllium copper for springs carrying electrical current (because of its low electrical resistance). When a spring is compressed or stretched, the force it exerts is proportional to its change in length.

II. OBJECTIVE

- i. Study the exiting design of helical spring of two wheeler (e.g. Hero Splendor 125 cc)
- ii. Model the existing design of spring in CATIA software& carry out analysis in ANSYS.
- iii. Carry out the test on existing design and compare with FEA results.
- iv. Reduce the diameter of spring and prepare two different designs.
- v. Analyse the new designs in ANSYS and compare the results with baseline model.
- vi. Propose the optimised design (cost effective and less weight) of spring for two-wheeler.

A. Problem Definition

Helical springs are the most important part in the two wheeler suspension system. Every organisation wants to reduce the cost of the material used in the different parts. Most of the time due to continuous loading, the spring manufacturer used more factor of safety to design the spring. But, keeping higher factor of safety, the cost of material used to manufacture

the spring becomes high. Therefore, our project aim is to keep minimum factor of safety for suitable operation of helical spring. The reduction in material leads to reduction in overall cost of the springs.





Figure 3.1 Methodology Flowchart

IV. SIMULATION

A. Material Properties

High-carbon spring steels are the most commonly used of all springs materials. This material is preferred to others because they are least expensive, readily available, easily worked, and most popular. These materials are not satisfactory for high or low temperatures or for shock or impact loading. Also this is the general purpose spring steels and should only be used where life accuracy and deflection are not too important.

1. Nominal Mechanical Properties

- Young's Modulus: 206000 MPa
- Modulus of Rigidity: 85000 MPa
- Density: 7800 kg/m³
- Poisson's Ratio: 0.33
- Tensile yield strength = 250 MPa

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| Parameter | Dimension |
|-------------------------|-----------|
| Upper outer diameter | 50 mm |
| Lower outer diameter | 50 mm |
| Height of the spring | 230 mm |
| Diameter of spring wire | 7 mm |
| Pitch | 8mm |





Figure 4.1 2D Drafting of Helical Spring - Baseline Design

B. Calculations

1. Baseline Helical Spring

a) Samplecalculation for the helical spring:

D= Mean Coil Diameter, mm = 43 mm

d= Wire Diameter, mm = 7 mm

N = number of active coils = 18

P = Axial force, N = 200Kg = 200 x 9.81 = 1962 N

- (1) Spring index, C=D/d=43/7=6.143
- (2) Wahl's stress factor, k = [(4C-1)/(14C-4)+(0.615/C)]k = 1.294
- (3) Maximum shear stress, $\tau = (k \times 8PD)/\pi d3$ $= (1.294 \text{ x } 8 \text{ x } 1962 \text{ x } 43)/(3.14 \text{ x } 7^3)$ $\tau = 810.9\text{MPa}.$
- (4) **Deflection of spring,** $\delta = 8 PD^3 N/Gd^4$ $\delta = (8 \times 1962 \times 43^3 \times 18)/(1.6e5 \times 7^{4)}$ $\delta = 58.47 \text{ mm.}$

2. New Design of Helical Spring



Figure 4.2 2D Drafting of the Design-Model-6mm

D= Mean Coil Diameter, mm = 43 mm d= Wire Diameter, mm = 6 mm N = number of active coils = 18 P = Axial force, N = 200Kg = 200 x 9.81 = 1962 N

- (1) **Spring index** C=D/d = 43/6 = 7.16
- (2) Wahl's stress factor, k = [(4C-1)/(14C-4) + (0.615/C)]k = 1.247
- (3) Maximum shear stress,

 $\tau = (k \times 8PD)/\pi d3$ = (1.247 x 8 x 1962 x 43)/ (3.14 x 6³) $\tau = 1240.9$ MPa.

(4) **Deflection of spring**,

 $\delta = 8PD^{3}N/Gd^{4}$ $\delta = (8 \times 1962 \times 43^{3} \times 18)/(1.6e5 \times 6^{4})$ $\delta = 108.32 \text{ mm.}$

C. Finite Element Analysis Approach

The finite element analysis includes pre-processing, solution and post processing. Following are the most important steps to be followed during analysis.

- CAD Modelling
- Pre-processing -
 - Importing CAD model in ANSYS
 - o Meshing,
 - Material Assignment,
 - Assigning element types,
 - Assigning loading and boundary conditions,
 - Assigning time steps
- Solution -
 - \circ Run the FEA model
- Post-processing -
 - Observe the displacement
 - o Observed animation of displacement
 - If animation is logical as per applied boundary conditions, then proceed to record stresses.
 - o Record von-Mises stress for all parts

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| MMMMMMMM | ANSYS R14.5 B: 6mm_Diameter Total Deformation Type: Total Deformation Unit mm Time: 1 Custom Max: 14.016 Min: 0 4/3/2017 12:26 AM 14.016 14.2459 10.901 9.3441 7.7668 6.2294 4.6721 3.1147 1.5574 0 | ANSYS Ridas |
|----------|--|----------------|
| | | • |

Figure IV.3 CAD Model – Diameter- 6mm Figure IV.4 Total Deformation Contour Plots Diameter-6mm



Figure IV.5 Von-Mises Stress Contour Plots Diameter-6mm Figure IV.6 Equivalent Elastic Strain Contour Plots Diameter-6mm

D. Summary Table (From Finite Element Analysis)

| Sr. | Description | Mass, Kg | Deflection, | Von-Mises |
|-----|-------------------|----------|-------------|-------------|
| No. | | | mm | stress, MPa |
| 1 | Baseline Design-1 | 0.711 | 6.99 | 204 |
| 2 | Design-2 | 0.535 | 14.02 | 280 |
| 3 | Design-3 | 0.379 | 30.44 | 340 |

 Table 4.2 Summary Table (From Finite Element Analysis)

| | Table 5.1 Experimental Readings | | | | | | | |
|-----|---------------------------------|----------|----------------|-------------|--|--|--|--|
| Sr. | Description | Mass, Kg | Deflection, mm | Von-Mises | | | | |
| No. | | | | stress, MPa | | | | |
| 1 | Baseline Design-1 | 0.711 | 8 | 210 | | | | |
| | | | 7 | | | | | |
| | | | 8 | | | | | |
| 2 | Design-2 | 0.535 | 15 | 300 | | | | |
| | | | 14 | | | | | |
| | | | 13 | | | | | |
| 3 | Design-3 | 0.379 | 35 | 380 | | | | |
| | | | 34 |] | | | | |
| | | | 32 | 1 | | | | |

V. EXPERIMENTAL VALIDATION Table 5.1 Experimental Readings

VI. RESULTS AND DISCUSSION

It is observed from the results that maximum stresses are developed at extreme ends of the helical spring. The maximum deformation in helical spring is observed up to 7 mm. The Von-Mises stress in the helical spring for the maximum load of 100 Kg is 204MPa. The total weight of the helical spring is 0.711 kg. Therefore, the von-mises stress in the spring is below their yield strength of the material. **Hence, there is maximum scope to reduce the mass of the suspension system in baseline design.**

| FEA | I | Design-1 | Design-2 | | Design-3 | |
|---|---|---|---|--|--|--|
| Time (s) | Load (N) | Deflection (mm) | Load (N) | Deflection (mm) | Load (N) | Deflection (mm) |
| 0.1 | 100 | 0.69926 | 100 | 1.4016 | 100 | 3.0448 |
| 0.2 | 200 | 1.3985 | 200 | 2.8032 | 200 | 6.0896 |
| 0.3 | 300 | 2.0978 | 300 | 4.2049 | 300 | 9.1343 |
| 0.4 | 400 | 2.7971 | 400 | 5.6065 | 400 | 12.179 |
| 0.5 | 500 | 3.4963 | 500 | 7.0081 | 500 | 15.224 |
| 0.6 | 600 | 4.1956 | 600 | 8.4097 | 600 | 18.269 |
| 0.7 | 700 | 4.8949 | 700 | 9.8113 | 700 | 21.313 |
| 0.8 | 800 | 5.5941 | 800 | 11.213 | 800 | 24.358 |
| 0.9 | 900 | 6.2934 | 900 | 12.615 | 900 | 27.403 |
| 1 | 1000 | 6.9926 | 1000 | 14.016 | 1000 | 30.448 |
| | | | | | | |
| | | | | | | |
| Experimental | I | Design-1 | I | Design-2 | I | Design-3 |
| Experimental Time (s) | I Load (N) | Design-1 Deflection (mm) | I Load (N) | Design-2 Deflection (mm) | I Load (N) | Design-3 Deflection (mm) |
| Experimental Time (s) 0.1 | I Load (N) 100 | Design-1 Deflection (mm) 0.8 | I Load (N) 100 | Design-2 Deflection (mm) 1.5 | I Load (N) 100 | Design-3 Deflection (mm) 3.5 |
| Experimental Time (s) 0.1 0.2 | I Load (N) 100 200 | Design-1 Deflection (mm) 0.8 1.6 | I Load (N) 100 200 | Design-2 Deflection (mm) 1.5 3 | I Load (N) 100 200 | Design-3 Deflection (mm) 3.5 7 |
| Experimental Time (s) 0.1 0.2 0.3 | Load (N) 100 200 300 | Design-1 Deflection (mm) 0.8 1.6 2.4 | Load (N) 100 200 300 | Design-2 Deflection (mm) 1.5 3 4.5 | Load (N) 100 200 300 | Design-3 Deflection (mm) 3.5 7 10.5 |
| Experimental Time (s) 0.1 0.2 0.3 0.4 | Load (N) 100 200 300 400 | Design-1 Deflection (mm) 0.8 1.6 2.4 3.2 | Load (N) 100 200 300 400 | Design-2 Deflection (mm) 1.5 3 4.5 6 | Load (N) 100 200 300 400 | Design-3 Deflection (mm) 3.5 7 10.5 14 |
| Experimental Time (s) 0.1 0.2 0.3 0.4 0.5 | Load (N) 100 200 300 400 500 | Design-1 Deflection (mm) 0.8 1.6 2.4 3.2 4 | Load (N) 100 200 300 400 500 | Design-2 Deflection (mm) 1.5 3 4.5 6 7.5 | Load (N) 100 200 300 400 500 | Design-3 Deflection (mm) 3.5 7 10.5 14 17.5 |
| Experimental Time (s) 0.1 0.2 0.3 0.4 0.5 0.6 | Load (N) 100 200 300 400 500 600 | Design-1 Deflection (mm) 0.8 1.6 2.4 3.2 4 4.8 | Load (N) 100 200 300 400 500 600 | Design-2 Deflection (mm) 1.5 3 4.5 6 7.5 9 | Load (N) 100 200 300 400 500 | Design-3 Deflection (mm) 3.5 7 10.5 14 17.5 21 |
| Experimental Time (s) 0.1 0.2 0.3 0.4 0.5 0.6 0.7 | Load (N) 100 200 300 400 500 600 700 | Design-1 Deflection (mm) 0.8 1.6 2.4 3.2 4 4.8 5.6 | Load (N) 100 200 300 400 500 600 700 | Design-2 Deflection (mm) 1.5 3 4.5 6 7.5 9 10.5 | Load (N) 100 200 300 400 500 600 700 | Design-3 Deflection (mm) 3.5 7 10.5 14 17.5 21 24.5 |
| Experimental Time (s) 0.1 0.2 0.3 0.4 0.5 0.6 0.7 0.8 | Load (N) 100 200 300 400 500 600 700 800 | Design-1 Deflection (mm) 0.8 1.6 2.4 3.2 4 4.8 5.6 6.4 | Load (N) 100 200 300 400 500 600 700 800 | Design-2 Deflection (mm) 1.5 3 4.5 6 7.5 9 10.5 12 | Load (N) 100 200 300 400 500 600 700 800 | Design-3 Deflection (mm) 3.5 7 10.5 14 17.5 21 24.5 28 |
| Experimental Time (s) 0.1 0.2 0.3 0.4 0.5 0.6 0.7 0.8 0.9 | Load (N) 100 200 300 400 500 600 700 800 900 | Design-1 Deflection (mm) 0.8 1.6 2.4 3.2 4 4.8 5.6 6.4 7.2 | Load (N) 100 200 300 400 500 600 700 800 900 | Design-2 Deflection (mm) 1.5 3 4.5 6 7.5 9 10.5 12 13.5 | Load (N) 100 200 300 400 500 600 700 800 900 | Design-3 Deflection (mm) 3.5 7 10.5 14 17.5 21 24.5 28 31.5 |

 Table 6.1 Deflection Results (FEA & Experimental)



Figure 6.1 Load Vs. Deflection (FEA & Exprerimental)

The maximum deformation in design-2 of helical spring is observed up to 14 mm. The Von-Mises stress in the helical spring for the maximum load of 100 Kg is 240MPa. The total weight of the helical spring is 0.535 kg. Therefore, the von-mises stress in the spring is below their yield strength of the material. **Hence, the design-2 is safe for the applied loading conditions.**

The maximum deformation in design-3 of helical spring is observed up to 30 mm. The Von-Mises stress in the helical spring for the maximum load of 100 Kg is 340MPa. The total weight of the helical spring is 0.379 kg. Therefore, the von-mises stress in the spring is above their yield strength of the material. But, the stresses are below their ultimate tensile strength of material. Hence, there are chances of permanent deformation of the design-3. Therefore, design-3 is not suitable for our application.

If we compare the masses of the three designs, the design-2 of the helical spring lighter than baseline design-1. The designs-2 is 25% lighter in weight than design-1.

The following table and graph shows values of Von-Mises stress for the Finite element analysis and Experimental setup for the helical spring.

| FEA | Design-1 | | Design-1 Design-2 | | Design-3 | |
|----------|-------------|--------------------------------|---|-----|-------------|--------------------------------|
| Time (s) | Load (N) | Stress (N/mm ²) | Load Stress (N) (N/mm ²) | | Load (N) | Stress (N/mm ²) |
| 0.1 | 100 | 20.4 | 100 | 28 | 100 | 34 |
| 0.2 | 200 | 40.8 | 200 | 56 | 200 | 68 |
| 0.3 | 300 | 61.2 | 300 | 84 | 300 | 102 |
| 0.4 | 400 | 81.6 | 400 | 112 | 400 | 136 |
| 0.5 | 500 | 102 | 500 | 140 | 500 | 170 |
| 0.6 | 600 | 122.4 | 600 | 168 | 600 | 204 |
| 0.7 | 700 | 142.8 | 700 | 196 | 700 | 238 |
| 0.8 | 800 | 163.2 | 800 | 224 | 800 | 272 |
| 0.9 | 900 | 183.6 | 900 | 252 | 900 | 306 |
| 1 | 1000 | 204 | 1000 | 280 | 1000 | 340 |
| | • | | • | • | • | • |

| Table 6.2 | Stress | Results | (FEA | & Ex | nerimental) |) |
|-----------|---------|-----------------|------|-------|-------------|---|
| 1 and 0.4 | 011 033 | I Coulto | | C L'A | pumunuar | , |

| Experimental | Des | sign-1 | Design-2 | | Des | Design-3 | |
|--------------|-------------|--------------------------------|-------------|--------------------------------|-------------|--------------------------------|--|
| Time (s) | Load (N) | Stress (N/mm ²) | Load (N) | Stress (N/mm ²) | Load (N) | Stress (N/mm ²) | |
| 0.1 | 100 | 21 | 100 | 30 | 100 | 38 | |
| 0.2 | 200 | 42 | 200 | 60 | 200 | 76 | |
| 0.3 | 300 | 63 | 300 | 90 | 300 | 114 | |
| 0.4 | 400 | 84 | 400 | 120 | 400 | 152 | |
| 0.5 | 500 | 105 | 500 | 150 | 500 | 190 | |
| 0.6 | 600 | 126 | 600 | 180 | 600 | 228 | |
| 0.7 | 700 | 147 | 700 | 210 | 700 | 266 | |
| 0.8 | 800 | 168 | 800 | 240 | 800 | 304 | |
| 0.9 | 900 | 189 | 900 | 270 | 900 | 342 | |
| 1 | 1000 | 210 | 1000 | 300 | 1000 | 380 | |



Figure 6.2 Load Vs Stress (FEA & Experimental)

VII. CONCLUSIONS

The comparative study of the suspension system helical coil spring with the three different designs has reached at the following conclusion:

- i. The deflection in modified design-2 of the helical spring is slightly higher than that of baseline design.
- ii. Maximum von-Misesstress is increase in a very minimal amount but, it is less than yield strength of material.
- iii. The mass of the design-2 is 25% lighter than baseline design-1.
- iv. Design -2 with wire diameter -6 mm is efficient for the applied loading conditions and stands out to be efficient design for spring especially at higher loads.
- v. Thus, stainless steel with design-2 is most suitable optimized design of helical spring for manufacturing.

VIII. NOMENCLATURE

- FEA Finite Element Analysis
- VSS Vehicle Suspension System
- CATIA Computer Aided Three-dimensional Interactive Application
- C Spring Index
- T Maximum Shear Stress
- Δ Deflection Of The Spring
- K Wahl's Stress Factor
- K Stiffness

REFERENCES

- 1. Christianah O. Ijagbemia, Bankole I. Oladapo, Design and simulation of fatigue analysis for a vehicle suspension system (VSS) and its effect on global warming, Procedia Engineering 159 (2016) 124 132
- 2. M.venkatesan, Design and analysis of composite leaf spring in light vehicle, ISSN: 2277-9655(I2OR).
- 3. Mr. J. J. Pharne, Design, analysis and experimental validation for fatigue behavior of a helical compression spring used for a two wheeler horn, International Journal of Mechanical and Industrial Engineering (IJMIE) ISSN No. 2231 –6477, Vol-2, Iss-3, 2012.
- 4. Mr.ChandrakantChavan, Analysis for suspension spring to determine and improve its fatigue life using finite element methodology, International Journal of Engineering and Computer Science ISSN: 2319-7242, Volume 4 Issue 3 March 2015.
- Tausif m. Mulla, sunil j. Kadam, vaibhav s. Kengar, Finite element analysis of helical coil compression spring for three wheeler automotive front suspension, International Journal of Mechanical and Industrial Engineering (IJMIE) ISSN No. 2231-6477, Vol-2, Iss-3, 2012.
- 6. Rajkumar V. Patil, Comparison of cylindrical and conical helical springs for theirBuckling load and deflection, International Journal of Mechanical and Industrial Engineering (IJMIE) ISSN No. 2231–6477, Vol-1, Iss-2, 2011.
- 7. B. D. Shiwalkar, Design Data for MachineElements. 2012 Edition, pp79-92.
- 8. R. S. Khurmi and J. K. Gupta, "MachineDesign", S. Chand publication, pp.820-844.