# SELECTION OF THE WIRE CUT ELECTRICAL DISCHARGE MACHINING PROCESS PARAMETERS USING GRA METHOD

Vipal B Patel<sup>1</sup>\*, Jaksan D. Patel<sup>2</sup>, Kalpesh D. Maniya<sup>3</sup>

<sup>1</sup>*M.E.* student, Sardar Patel Institute of Technology, Piludara, Mehsana, vipalpatel87@gmail.com <sup>2</sup>*Head of Mechanical Department at Merchant Polytechnic, Basna, pateljaksan\_mech1986@yahoo.com* <sup>3</sup>*Asst. Professor, C.K.Pithawalla College of engg. & Technology, Surat, maniya777@yahoo.co.in* 

**Abstract**: Wire electrical discharge machining (WEDM) is one of the important non-traditional machining processes, which is used for machining of difficult-to-machine materials and intricate profiles. WEDM is a complex machining process controlled by a large number of process parameters such as Pulse on Time (Ton), Pulse off Time (Toff), Flushing Pressure (FP), Wire Tension (Wt), Servo Voltage (SV) and Wire Feed Rate (WF) in Wire Cut Electrical Discharge Machining (WEDM) Operations. The Response Process Parameters are measure in Wire Cut Electrical Discharge Machining (WEDM) Operations Such as Material Removal Rate, Kerf Width and Surface Roughness have been considered for Each Experiment. Experimentation was planned as per Taguchi's L27 Orthogonal array. Molybdenum Wire with 0.25 mm Diameter and High Carbon High Chromium Die Steel (HCHCR) were used as tool and Work Materials in the Experiments. The Machining parameters are optimized with the multi response characteristics of the material removal, kerf width rate and surface roughness using the grey relational analysis.

Keywords: WEDM, Step by Step Procedure of WEDM, Taguchi Method, Orthogonal Array, GRA

## **I.INTRODUCTION**

One of the most widely used Non-Conventional Machining process in industry is Electrical Discharge Machining (EDM)[1]. Electric Discharge Machining is a non- traditional concept which is based on the principle of removing material by means of repeated electrical discharges between the tool termed as electrode and the work piece in the presence of a dielectric fluid. WEDM is considered as a unique adoption of the conventional EDM process which comprises of a main worktable, wire drive mechanism, a CNC controller, working fluid tank and attachments. The work piece is placed on the fixture table and fixed securely by clamps and bolts. The table moves along X and Y-axis and it is driven by the DC servo motors. Wire electrode usually made of thin copper, brass, molybdenum or tungsten of diameter 0.05-0.30 mm, which transforms electrical energy to thermal energy, is used for cutting materials. The wire is stored and wound on a wire drum which can rotate at1500rpm. The wire is continuously fed from wire drum which moves though the work piece and is supported under tension between a pair of wire guides located at the opposite sides of the work piece. During the WEDM process, the material is eroded ahead of the wire and there is no direct contact between the work piece and the wire, eliminating the mechanical stresses during machining. Also the work piece and the wire electrode (tool) are separated by a thin film of dielectric fluid that is continuously fed to the machining zone to flush away the eroded particles. The movement of table is controlled numerically to achieve the desired three-dimensional shape and accuracy of the work piece [1].

# A. STEP BY STEP PROCEDUREOFWEDMPROCESS:

Step: 1

Generation of Volts and Amps as wire is surrounded by deionized water as shown in figure 1.1 [2].



"Figure: 1.1 Volts and Amps produced by power supply [2]"

# Step: 2

During pulse on time controlled sparks are produced between work piece and electrode which helps in erosion and hence precisely melts and vaporize the material as shown in figure 1.2.



"Figure: 1.2Sparkgeneration and erosion of material [2]"

# Step: 3

During pulse off time pressurized dielectric fluid cools the material and flushes away the eroded particles as shown in figure 1.3.



"Figure: 1.3Flushing of corroded particles [2]"

## Step: 4

A filter system is used to filter the eroded particles from the dielectric fluid and the fluid is thus reused as shown in figure 1.4.



"Figure: 1.4Filtration and reuse of dielectric [2]"

# **II. LITERATURESURVEY**

# A.LITERATURE REVIEW: BASED ON WEDM:

N.Tosun et. al. employed Taguchi's approach to investigate and optimize the effects of dielectric flushing pressure, pulse duration, wire speed and open circuit voltage on kerf and MRR for AISI 4140 steel and inferred that the highly significant factors for both, the MRR

and the kerf, are open voltage and pulse duration whereas dielectric flushing pressure and wire speed are less effective factors. It has also concluded that confirmation tests indicated that it is possible to decrease kerf and increase MRR significantly by using the proposed statistical technique. [3]

- Kanlayasiri and Boonmung have investigated influences of wire-EDM machining variables on surface roughness of newly developed DC 53 die steel of width, length, and thickness 27, 65 and 13 mm, respectively. The machining variables included pulse-on time, pulse-off time, pulse-peak current, and wire tension. The variables affecting the surface roughness were identified using ANOVA technique. Results showed that pulse-on time and pulse-peak current were significant variables to the surface roughness of wire- EDM DC53 die steel. The maximum prediction error of the model was less than 7% and the average percentage error of prediction was less than 3%. [4].
- B.K. Nanda et. al. have conducted the experiment on Parametric Optimization of CNC Wire Cut Electrical Discharge Machining using grey relational Analysis. In This Experiment has been performed under different cutting conditions with the grey relational Analysis and analysis of variance (ANOVA). Grey relational grade using the optimal process parameter combinations and found that a good agreement between the predicted and actual grey relational grade. The increase of grey relational grade from initial factor setting to the optimal process parameter setting is of 0.1275. It has concluded that optimization of the complicated multiple performance characteristics using gray relation method and obtain the material removal rate, surface roughness are improved together.[5]
- Datta and Mahapatra have proposed a quadratic mathematical model and conducted experiments by taking six WEDM process parameters: discharge current, pulse duration, pulse frequency, wire speed, wire tension and dielectric flow rate. Experiments were carried out on D2 Tool Steel using a Zinc coated Copper wire electrode. The response parameters noticed for each experiment were MRR, Surface Roughness and Kerf. A statistical analysis has been carried for each result and responses have been utilized to fit the quadratic model which represents the above said six parameters. Grey based Taguchi technique has been utilized to evaluate optimal parameter combination to achieve maximum MRR, minimum roughness value and minimum width of cut; with selected experimental domain. It has been found out that for continuous quality improvement Grey based Taguchi method is a very reliable method to predict optimal parameter values and all the parameters involved in the experimentation are independent of each other.[6]
- Pasam et. al. have developed a mathematical model by using linear regression analysis in order to present a relationship between control parameters and response parameters. Titanium alloy is chosen as work piece material. Control parameters which have been varied are Ignition pulse current, Short pulse duration, Time between two pulses, Servo speed, Servo voltage, Injection pressure, Wire speed and Wire tension and the response parameter studied for the above parameters is surface roughness. Genetic algorithm modelling has been used to optimize the process parameters for surface roughness. Regression coefficient of 0.943 is obtained for surface roughness model by regression analysis and surface roughness of 1.85 µm is obtained with selected optimum control parameters in the WEDM of Ti6A44V alloy.[7]
- Kuo-Wei Lin et. al. have conduct test Wire Electrical Discharge Machining (WEDM) of magnesium alloy parts via the taguchi method-based gray analysis was conducted; they

considered multiple quality characteristics required include material removal rate and surface roughness following WEDM. Entropy Weighting employs the entropy concept to determine the relative weighting factor for each attribute. This work machines magnesium alloy parts under controlled machine parameter settings, and measures the above quality characteristics. The optimized machine parameter settings clearly improve quality characteristics of the machined work piece compared to quality levels achieved for initial machine parameter settings. The complex interactions in WEDM involve wire feed rate, pulse-on time, pulse-off time, no load voltage, servo voltage, and wire tension.[8]

C Bhaskar Reddy et.al. also conducted the experiments in wire EDM based on L16 Orthogonal array selecting EN19 and SS420 steel as work material with 0.18 mm Molybdenum wire as electrode. The experiments are conducted considering the above two materials for L16 and then the impact of each parameter is estimated by ANOAVA. Then the regression analysis is carried-out to find the trend of the response of each material. Recommend better parameter settings to achieve higher MRR and better surface roughness. Based on the results; it is recommended that the EN 19 material is suitable for better MRR. Then the SS 420 material is recommended to obtain better surface. [9].

## **III. DESIGN OF EXPERIMENT BASED ON TAGUCHI METHOD:**

The experimental layout for the machining parameters using the L27 orthogonal array was used in this study. This array consists of six control parameters and three levels. Minitab automatically creates the design and stores it in the worksheet.

| Mac | hining Process Parameters   | Level 1 | Level 2 | Level 3 |
|-----|-----------------------------|---------|---------|---------|
| 1   | Pulse On Time (µs)          | 115     | 120     | 125     |
| 2   | Pulse Off Time (µs)         | 45      | 50      | 55      |
| 3   | Flushing pressure (kgf/cm2) | 10      | 12      | 14      |
| 4   | Wire Tension(gms)           | 600     | 900     | 1200    |
| 5   | Servo Voltage (volt)        | 20      | 25      | 30      |
| 6   | Wire Feed Rate (m/min)      | 4       | 6       | 8       |

"Table No: 1.1 Input Variables with Different Levels"

"Table No: 1.2 Experimental Design Using L27 Orthogonal Array"

| Exp.<br>No | Ton<br>(µs) | Toff<br>(µs) | Fp<br>(Kgf/<br>cm2) | Wt<br>(gms) | SV<br>(volt) | Wf<br>(m/min) | MRR<br>(mm3/<br>min) | KW<br>(mm) | SR<br>(µm) |
|------------|-------------|--------------|---------------------|-------------|--------------|---------------|----------------------|------------|------------|
| 1          | 115         | 45           | 10                  | 600         | 20           | 4             | 6.3682               | 0.2565     | 2.498      |
| 2          | 115         | 45           | 10                  | 600         | 25           | 6             | 6.2817               | 0.2585     | 2.458      |
| 3          | 115         | 45           | 10                  | 600         | 30           | 8             | 5.9658               | 0.2604     | 2.335      |
| 4          | 115         | 50           | 12                  | 900         | 20           | 4             | 5.6581               | 0.2585     | 2.807      |
| 5          | 115         | 50           | 12                  | 900         | 25           | 6             | 5.5327               | 0.2623     | 2.812      |
| 6          | 115         | 50           | 12                  | 900         | 30           | 8             | 5.5937               | 0.2711     | 2.714      |

| 7  | 115 | 55   | 14   | 1200  | 20     | 4       | 5.2816  | 0.2665   | 2.786 |
|----|-----|------|------|-------|--------|---------|---------|----------|-------|
| 8  | 115 | 55   | 14   | 1200  | 25     | 6       | 5.1930  | 0.2724   | 2.680 |
| 9  | 115 | 55   | 14   | 1200  | 30     | 8       | 5.1124  | 0.2764   | 2.763 |
| 10 | 120 | 45   | 12   | 1200  | 20     | 6       | 8.3161  | 0.2700   | 3.375 |
| 11 | 120 | 45   | 12   | 1200  | 25     | 8       | 7.9069  | 0.2677   | 3.403 |
| 12 | 120 | 45   | 12   | 1200  | 30     | 4       | 7.4141  | 0.2661   | 3.370 |
| 13 | 120 | 50   | 14   | 600   | 20     | 6       | 7.1922  | 0.2702   | 3.399 |
| 14 | 120 | 50   | 14   | 600   | 25     | 8       | 6.9960  | 0.2716   | 3.434 |
| 15 | 120 | 50   | 14   | 600   | 30     | 4       | 7.0043  | 0.2813   | 3.417 |
| 16 | 120 | 55   | 10   | 900   | 20     | 6       | 5.8348  | 0.2589   | 3.470 |
| 17 | 120 | 55   | 10   | 900   | 25     | 8       | 5.3332  | 0.2550   | 3.504 |
| 18 | 120 | 55   | 10   | 900   | 30     | 4       | 5.0727  | 0.2552   | 3.388 |
| 19 | 125 | 45   | 14   | 900   | 20     | 8       | 8.4101  | 0.2623   | 3.536 |
| 20 | 125 | 45   | 14   | 900   | 25     | 4       | 8.1089  | 0.2638   | 3.485 |
| 21 | 125 | 45   | 14   | 900   | 30     | 6       | 8.1004  | 0.2656   | 3.450 |
| 22 | 125 | 50   | 10   | 1200  | 20     | 8       | 7.6840  | 0.2589   | 3.505 |
| 23 | 125 | 50   | 10   | 1200  | 25     | 4       | 7.4889  | 0.2616   | 3.489 |
| 24 | 125 | 50   | 10   | 1200  | 30     | 6       | 7.7415  | 0.2758   | 3.429 |
| 25 | 125 | 55   | 12   | 600   | 20     | 8       | 7.2994  | 0.2759   | 3.427 |
| 26 | 125 | 55   | 12   | 600   | 25     | 4       | 7.0054  | 0.2808   | 3.446 |
| 27 | 125 | 55   | 12   | 600   | 30     | 6       | 7.1029  | 0.2936   | 3.399 |
|    | Ι   | V.ME | THOD | )LOGY | : GREY | RELATIO | ON ANAI | LYSIS (G | (RA)  |

In grey relational analysis, the function of factors is neglected in situations where the range of the sequence is large or the standard value is enormous .However, this analysis might produce incorrect results if the factors ,goal and directions are different .Therefore one has to pre-process the data which are related to a group of sequence ,which is called "grey relational generation "data preprocessing is a process of transferring the original sequence to a comparable sequence for this purpose the experimental result are normalized in the range between zero and one the normalization can be done from three different approaches.

# A. Data pre-processing

If the target value of original sequence is infinite, then it has a characteristic of "the larger the better".

The original sequence can be normalized as follows [5]:

$$X_{i}(k) = \frac{Y_{i}(k) - \min Y_{i}(k)}{\max Y_{i}(k) - \min Y_{i}(k)}$$

If the expectancy is "the smaller the better" than the original sequence should be normalized as follows:

$$Xi(k) = \frac{maxYi(k)-Yi(k)}{maxYi(k)-minYi(k)} \qquad \dots \qquad \text{Eq.2}$$

Here X (k) i is the value after grey relational generation [5], min y (k) i is the smallest value of y (k) i for the k<sup>th</sup> response, and max y (k) i is the largest value of y (k) i for the k<sup>th</sup> response. An ideal sequence is (1, 2, 3... 27) 0 x k, k = for the responses. The definition of grey relational grade in the course of grey relational analysis is to reveal the degree of relation between the 27 sequences ,(1,2,3,...,27) 0 x k and x k, k = i.

# **B.** Grey relational coefficient and Grey relational grade

Following data pre-processing, a grey relational coefficient is calculated to express the relationship between the ideal and actual normalized experimental results. The Grey relation coefficient [5] can be express as follows.

$$\zeta_{i}(k) = \frac{\Delta \min + \psi \Delta \max}{\Delta_{0i}(k) + \psi \Delta \max} \dots Eq.3$$

Where  $\Delta_{0i}^{(k)}$  is the deviation sequence of the reference sequence xi(k) and the comparability sequence.  $\Psi$  = distinguishing or identification coefficient in between zero and one.

$$\Delta_{0i} = \begin{vmatrix} \mathbf{x}_{0}(\mathbf{k}) - \mathbf{x}_{i}(\mathbf{k}) \end{vmatrix} \dots \dots \dots \text{Eq.4}$$
  
$$\Delta_{min} = \min_{i \in I} \min_{\mathbf{k}} \begin{vmatrix} \mathbf{x}_{0}(\mathbf{k}) - \mathbf{x}_{i}(\mathbf{k}) \end{vmatrix} \dots \dots \dots \text{Eq.5}$$
  
$$\Delta_{max} = \max_{i \in I} \max_{\mathbf{k}} \begin{vmatrix} \mathbf{X}_{0}(\mathbf{k}) - \mathbf{X}_{i}(\mathbf{k}) \end{vmatrix} \dots \dots \text{Eq.6}$$

After obtaining the Grey relation coefficient, its average is calculated to obtain the Grey relation grade. The Grey relation grade [5] is defined as follows:

$$\gamma_{i} = \frac{1}{n} \sum_{k=1}^{n} \zeta_{i}(k)$$
.....Eq.7

However, since in real application the effect of each factor on the system is not exactly same, Eq.7 can be modified as:

$$\gamma_i = \frac{1}{n} \sum_{k=1}^n W_k \zeta i(k)$$
.....Eq.8

Where Wk represents the normalized weighting value of factor k.

In Grey relation analysis, the grey relation grade is used to show the relationship among the sequences. If the two sequences are identical, then the value of Grey relation grade is equal to 1. The Grey relation grade also indicates the degree of influence that the comparability sequence could exert over the reference sequence. Therefore, if a particular comparability sequence is more important than the other comparability sequence to reference sequence will be higher than other grey relation grades. In this study, the importance of both the comparability sequence and reference sequence is treated as equal.

## V.ILLUSTRATE EXAMPLE:

Optimal parameter combination the work-piece kerf width, material removal rate and surface roughness for different combinations of WEDM parameter of 27 experimental runs are listed in table no: 1.3. It is concerned the lower surface roughness, the lower kerf width and the higher material removal rate are indications of better performance.

# "Table No: 1.3 Experimental results for material removal rate, kerf width and surface roughness"

| Exp.<br>No | Ton<br>(µs) | Toff<br>(µs) | Fp<br>(Kgf/<br>cm2) | Wt<br>(gms) | SV<br>(volt) | Wf<br>(m/min) | MRR<br>(mm3/<br>min) | KW<br>(mm) | SR<br>(µm) |
|------------|-------------|--------------|---------------------|-------------|--------------|---------------|----------------------|------------|------------|
| 1          | 115         | 45           | 10                  | 600         | 20           | 4             | 6.3682               | 0.2565     | 2.498      |
| 2          | 115         | 45           | 10                  | 600         | 25           | 6             | 6.2817               | 0.2585     | 2.458      |
| 3          | 115         | 45           | 10                  | 600         | 30           | 8             | 5.9658               | 0.2604     | 2.335      |
| 4          | 115         | 50           | 12                  | 900         | 20           | 4             | 5.6581               | 0.2585     | 2.807      |
| 5          | 115         | 50           | 12                  | 900         | 25           | 6             | 5.5327               | 0.2623     | 2.812      |
| 6          | 115         | 50           | 12                  | 900         | 30           | 8             | 5.5937               | 0.2711     | 2.714      |
| 7          | 115         | 55           | 14                  | 1200        | 20           | 4             | 5.2816               | 0.2665     | 2.786      |
| 8          | 115         | 55           | 14                  | 1200        | 25           | 6             | 5.1930               | 0.2724     | 2.680      |
| 9          | 115         | 55           | 14                  | 1200        | 30           | 8             | 5.1124               | 0.2764     | 2.763      |
| 10         | 120         | 45           | 12                  | 1200        | 20           | 6             | 8.3161               | 0.2700     | 3.375      |
| 11         | 120         | 45           | 12                  | 1200        | 25           | 8             | 7.9069               | 0.2677     | 3.403      |
| 12         | 120         | 45           | 12                  | 1200        | 30           | 4             | 7.4141               | 0.2661     | 3.370      |
| 13         | 120         | 50           | 14                  | 600         | 20           | 6             | 7.1922               | 0.2702     | 3.399      |
| 14         | 120         | 50           | 14                  | 600         | 25           | 8             | 6.9960               | 0.2716     | 3.434      |
| 15         | 120         | 50           | 14                  | 600         | 30           | 4             | 7.0043               | 0.2813     | 3.417      |
| 16         | 120         | 55           | 10                  | 900         | 20           | 6             | 5.8348               | 0.2589     | 3.470      |
| 17         | 120         | 55           | 10                  | 900         | 25           | 8             | 5.3332               | 0.2550     | 3.504      |
| 18         | 120         | 55           | 10                  | 900         | 30           | 4             | 5.0727               | 0.2552     | 3.388      |
| 19         | 125         | 45           | 14                  | 900         | 20           | 8             | 8.4101               | 0.2623     | 3.536      |
| 20         | 125         | 45           | 14                  | 900         | 25           | 4             | 8.1089               | 0.2638     | 3.485      |
| 21         | 125         | 45           | 14                  | 900         | 30           | 6             | 8.1004               | 0.2656     | 3.450      |
| 22         | 125         | 50           | 10                  | 1200        | 20           | 8             | 7.6840               | 0.2589     | 3.505      |

| 23 | 125 | 50 | 10 | 1200 | 25 | 4 | 7.4889 | 0.2616 | 3.489 |
|----|-----|----|----|------|----|---|--------|--------|-------|
| 24 | 125 | 50 | 10 | 1200 | 30 | 6 | 7.7415 | 0.2758 | 3.429 |
| 25 | 125 | 55 | 12 | 600  | 20 | 8 | 7.2994 | 0.2759 | 3.427 |
| 26 | 125 | 55 | 12 | 600  | 25 | 4 | 7.0054 | 0.2808 | 3.446 |
| 27 | 125 | 55 | 12 | 600  | 30 | 6 | 7.1029 | 0.2936 | 3.399 |

Table No 1.4 lists all of the sequences following data pre-processing kerf-width, material removal rate and surface roughness by using Eq.1 and Eq.2.

$$\begin{split} \mathbf{X}i(\mathbf{k}) &= \frac{\mathbf{Y}i(\mathbf{k}) - \min \mathbf{Y}i(\mathbf{k})}{\max \mathbf{Y}i(\mathbf{k}) - \min \mathbf{Y}i(\mathbf{k})} \dots \text{Eq.1} \\ \mathbf{X}i(\mathbf{k}) &= \frac{\max \mathbf{Y}i(\mathbf{k}) - \mathbf{Y}i(\mathbf{k})}{\max \mathbf{Y}i(\mathbf{k}) - \min \mathbf{Y}i(\mathbf{k})} \dots \text{Eq.2} \end{split}$$

"Table No: 1.4 Data Pre –Processing"

| Data Pre Processing |        |        |        |  |  |  |
|---------------------|--------|--------|--------|--|--|--|
| Exp.No              | MRR    | KW     | SR     |  |  |  |
| 1                   | 0.3882 | 0.9611 | 0.8643 |  |  |  |
| 2                   | 0.3623 | 0.9106 | 0.8980 |  |  |  |
| 3                   | 0.2676 | 0.8601 | 1.0000 |  |  |  |
| 4                   | 0.1754 | 0.9106 | 0.6074 |  |  |  |
| 5                   | 0.1378 | 0.8109 | 0.6028 |  |  |  |
| 6                   | 0.1561 | 0.5829 | 0.6848 |  |  |  |
| 7                   | 0.0626 | 0.7021 | 0.6245 |  |  |  |
| 8                   | 0.0360 | 0.5505 | 0.7132 |  |  |  |
| 9                   | 0.0119 | 0.4456 | 0.6440 |  |  |  |
| 10                  | 0.9718 | 0.6114 | 0.1341 |  |  |  |
| 11                  | 0.8492 | 0.6710 | 0.1112 |  |  |  |
| 12                  | 0.7015 | 0.7137 | 0.1382 |  |  |  |
| 13                  | 0.6351 | 0.6075 | 0.1145 |  |  |  |
| 14                  | 0.5763 | 0.5699 | 0.0853 |  |  |  |
| 15                  | 0.5788 | 0.3199 | 0.0995 |  |  |  |
| 16                  | 0.2284 | 0.8990 | 0.0550 |  |  |  |
| 17                  | 0.0781 | 1.0000 | 0.0266 |  |  |  |
| 18                  | 0.0000 | 0.9948 | 0.1232 |  |  |  |
| 19                  | 1.0000 | 0.8109 | 0.0000 |  |  |  |
| 20                  | 0.9098 | 0.7733 | 0.0425 |  |  |  |
| 21                  | 0.9072 | 0.7254 | 0.0716 |  |  |  |
| 22                  | 0.7824 | 0.8990 | 0.0262 |  |  |  |
| 23                  | 0.7240 | 0.8290 | 0.0391 |  |  |  |
| 24                  | 0.7997 | 0.4611 | 0.0889 |  |  |  |
| 25                  | 0.6672 | 0.4585 | 0.0912 |  |  |  |

| 26 | 0.5791 | 0.3316 | 0.0749 |
|----|--------|--------|--------|
| 27 | 0.6083 | 0.0000 | 0.1140 |

Also, the deviation sequences  $\Delta o_i$ ,  $\Delta max$  (k), and  $\Delta min$  (k) for i=1-27 and k=1-3 can be calculated as follows:

 $\Delta_{01} (1) = |\mathbf{X}_0 (1) - \mathbf{X}_1(1)| = |1.0000 - 0.3882| = 0.6118$  $\Delta_{01} (2) = |\mathbf{X}_0 (2) - \mathbf{X}_1(2)| = |1.0000 - 0.9611| = 0.0389$  $\Delta_{01} (3) = |\mathbf{X}_0 (3) - \mathbf{X}_1(3)| = |1.0000 - 0.8643| = 0.1357$ 

| The Deviation Sequence |        |        |        |  |  |  |  |
|------------------------|--------|--------|--------|--|--|--|--|
| Exp.No                 | 1.MRR  | 2.KW   | 3.SR   |  |  |  |  |
| 1                      | 0.6118 | 0.0389 | 0.1357 |  |  |  |  |
| 2                      | 0.6377 | 0.0894 | 0.1020 |  |  |  |  |
| 3                      | 0.7324 | 0.1399 | 0.0000 |  |  |  |  |
| 4                      | 0.8246 | 0.0894 | 0.3926 |  |  |  |  |
| 5                      | 0.8622 | 0.1891 | 0.3972 |  |  |  |  |
| 6                      | 0.8439 | 0.4171 | 0.3152 |  |  |  |  |
| 7                      | 0.9374 | 0.2979 | 0.3755 |  |  |  |  |
| 8                      | 0.9640 | 0.4495 | 0.2868 |  |  |  |  |
| 9                      | 0.9881 | 0.5544 | 0.3560 |  |  |  |  |
| 10                     | 0.0282 | 0.3886 | 0.8659 |  |  |  |  |
| 11                     | 0.1508 | 0.3290 | 0.8888 |  |  |  |  |
| 12                     | 0.2985 | 0.2863 | 0.8618 |  |  |  |  |
| 13                     | 0.3649 | 0.3925 | 0.8855 |  |  |  |  |
| 14                     | 0.4237 | 0.4301 | 0.9147 |  |  |  |  |
| 15                     | 0.4212 | 0.6801 | 0.9005 |  |  |  |  |
| 16                     | 0.7716 | 0.1010 | 0.9450 |  |  |  |  |
| 17                     | 0.9219 | 0.0000 | 0.9734 |  |  |  |  |
| 18                     | 1.0000 | 0.0052 | 0.8768 |  |  |  |  |
| 19                     | 0.0000 | 0.1891 | 1.0000 |  |  |  |  |
| 20                     | 0.0902 | 0.2267 | 0.9575 |  |  |  |  |
| 21                     | 0.0928 | 0.2746 | 0.9284 |  |  |  |  |
| 22                     | 0.2176 | 0.1010 | 0.9738 |  |  |  |  |
| 23                     | 0.2760 | 0.1710 | 0.9609 |  |  |  |  |
| 24                     | 0.2003 | 0.5389 | 0.9111 |  |  |  |  |
| 25                     | 0.3328 | 0.5415 | 0.9088 |  |  |  |  |
| 26                     | 0.4209 | 0.6684 | 0.9251 |  |  |  |  |
| 27                     | 0.3917 | 1.0000 | 0.8860 |  |  |  |  |

"Table No: 1.5the Deviation Sequences"

Using Table No: 1.5  $\Delta$ max and  $\Delta$ min can be found as follows.

 $\Delta_{\text{max}} = \Delta_{18} (1) = \Delta_{27} (1) = \Delta_{19} (1) = 1.0000$ 

$$\Delta_{\min} = \Delta_{19} (1) = \Delta_{17} (1) = \Delta_{03} (1) = 0.0000$$

The distinguishing coefficient can be substituted for the grey relational coefficient in Eq.3. Table 1.6 lists the grey relational coefficient and grade for each experiment of the L<sub>27</sub> Orthogonal array by applying Eq.8.Here weightage of each output parameters are calculated using Analytical hierarchy process.  $\Psi$  = distinguishing or identification coefficient is 0.5.

$$\zeta_{i}(k) = \frac{\Delta \min + \psi \Delta \max}{\Delta_{0i}(k) + \psi \Delta \max}$$
.....Eq.3

$$\gamma_i = \frac{1}{n} \sum_{k=1}^n W_k \zeta i(k)$$
.....Eq.8

"Table 1.6 Calculated Grey relational coefficient and Grey relational grade

| And its 27 | ' comparability | sequences" |
|------------|-----------------|------------|
|------------|-----------------|------------|

|        | Gr     | ey Relatio  | nal    | Cross relational |       |  |
|--------|--------|-------------|--------|------------------|-------|--|
| SR.NO  | C      | coefficient | S      | Grey relational  | Order |  |
|        | MRR    | KW          | SR     | grade            |       |  |
| WEIGHT | 0.5469 | 0.1085      | 0.3445 | -                | -     |  |
| 1      | 0.2459 | 0.1007      | 0.2710 | 0.6176           | 7     |  |
| 2      | 0.2403 | 0.0920      | 0.2861 | 0.6185           | 6     |  |
| 3      | 0.2219 | 0.0848      | 0.3445 | 0.6512           | 5     |  |
| 4      | 0.2064 | 0.0920      | 0.1930 | 0.4915           | 15    |  |
| 5      | 0.2007 | 0.0787      | 0.1920 | 0.4715           | 18    |  |
| 6      | 0.2035 | 0.0592      | 0.2113 | 0.4739           | 17    |  |
| 7      | 0.1902 | 0.0680      | 0.1967 | 0.4550           | 23    |  |
| 8      | 0.1868 | 0.0571      | 0.2189 | 0.4628           | 22    |  |
| 9      | 0.1838 | 0.0515      | 0.2012 | 0.4364           | 24    |  |
| 10     | 0.5177 | 0.0611      | 0.1261 | 0.7049           | 2     |  |
| 11     | 0.4202 | 0.0654      | 0.1240 | 0.6097           | 8     |  |
| 12     | 0.3425 | 0.0690      | 0.1265 | 0.5380           | 12    |  |
| 13     | 0.3161 | 0.0608      | 0.1243 | 0.5013           | 14    |  |
| 14     | 0.2960 | 0.0583      | 0.1218 | 0.4761           | 16    |  |
| 15     | 0.2968 | 0.0460      | 0.1230 | 0.4658           | 20    |  |
| 16     | 0.2150 | 0.0903      | 0.1192 | 0.4245           | 25    |  |
| 17     | 0.1923 | 0.1085      | 0.1169 | 0.4177           | 26    |  |
| 18     | 0.1823 | 0.1074      | 0.1251 | 0.4148           | 27    |  |
| 19     | 0.5469 | 0.0787      | 0.1148 | 0.7404           | 1     |  |
| 20     | 0.4633 | 0.0747      | 0.1182 | 0.6561           | 3     |  |
| 21     | 0.4613 | 0.0700      | 0.1206 | 0.6519           | 4     |  |
| 22     | 0.3811 | 0.0903      | 0.1169 | 0.5882           | 9     |  |



"Figure 1.5 Graph of Grey relational grades"

#### **VI. CONCLUSION**

In this work, a GRA based on the Taguchi method is used to directly integrate three WEDM cutting quality characteristics of (HCHCR) steel into a grey relational grade. The grade obtained for each experiment can immediately reflect the actual cutting results, including the surface roughness, Material removal rate and kerf width. An optimal combination of cutting parameters and the effect of each cutting parameter is obtained. According to performed experimental design, it is clearly observed from Table 1.6 and the Grey relational grade graph (Figure 1.5) which shows the change in the response when the 19 experiment gives the best multi- performance characteristics of the WEDM process among the 27 experiments.

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